

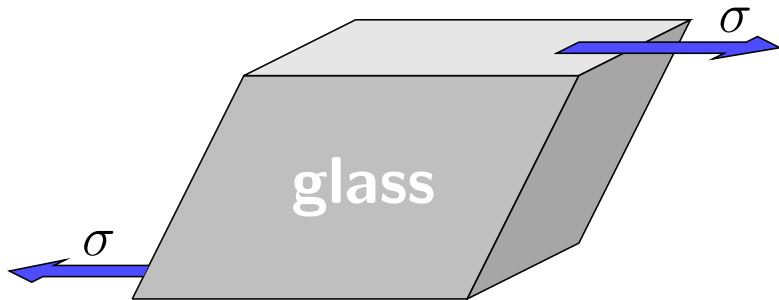
# Nonlinear plastic modes – micromechanics and statistics

Edan Lerner

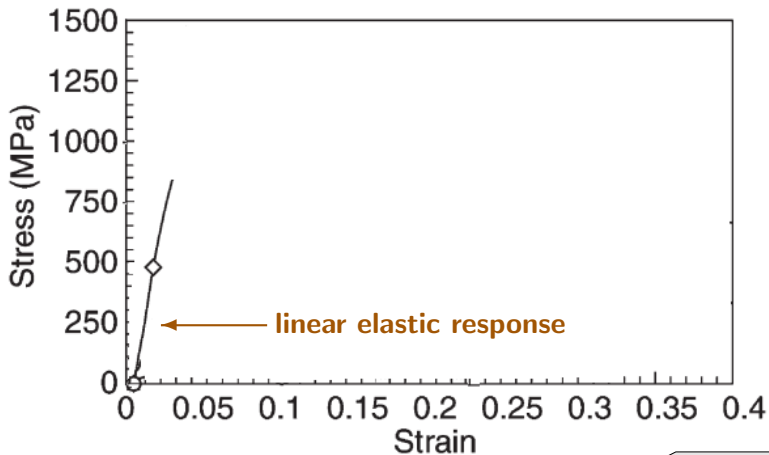
Institute for Theoretical Physics  
University of Amsterdam

yielding of amorphous solids  
ENS Paris  
Oct 2017

**what happens when a glass is deformed?**

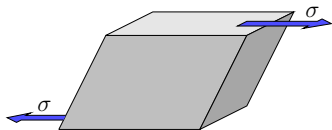


# elasto-plasticity – macroscopic response & yielding

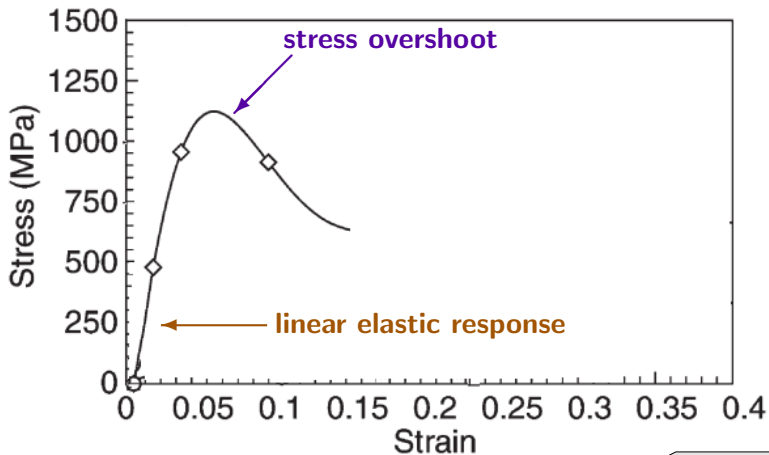


**'Vitreloy 1' (metallic glass)**

J. Lu, G. Ravichandran, W. Johnson, *Acta Materialia* 51 (2003)

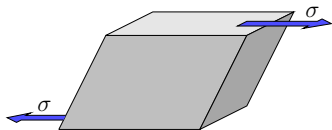


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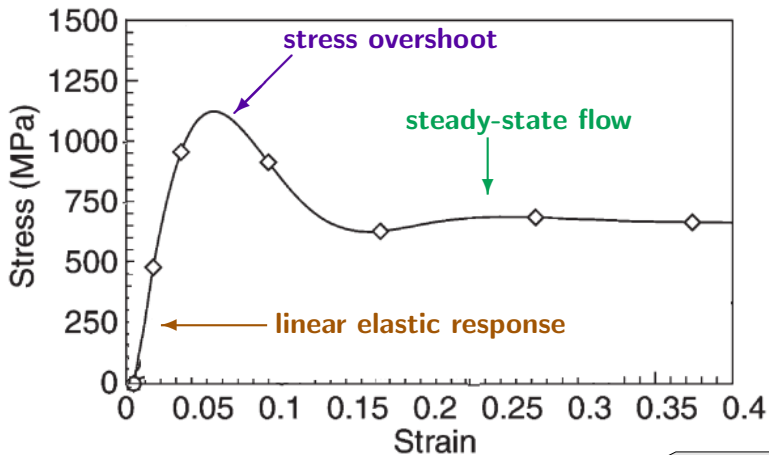


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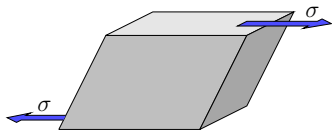


# elasto-plasticity – macroscopic response & yielding



**'Vitreloy 1' (metallic glass)**

J. Lu, G. Ravichandran, W. Johnson, Acta Materialia 51 (2003)



# what do we want to find?

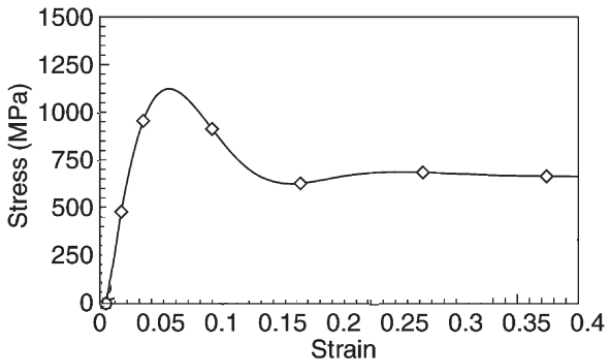
goal: theory for

$\sigma \equiv$  stress

$\dot{\gamma} \equiv$  deformation rate

$T \equiv$  Temperature

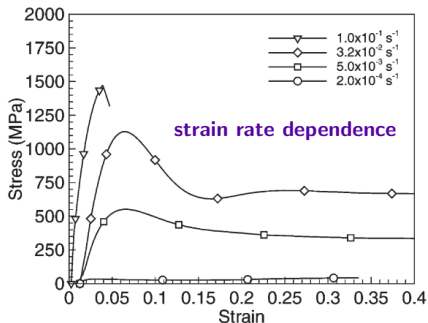
$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, \dots)$$



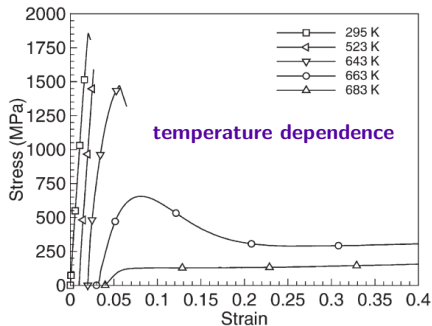
## experiments, metallic glass

J. Lu, G. Ravichandran, W. Johnson, *Acta Materialia* 51 (2003)

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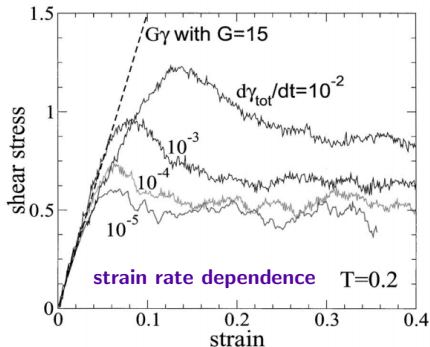
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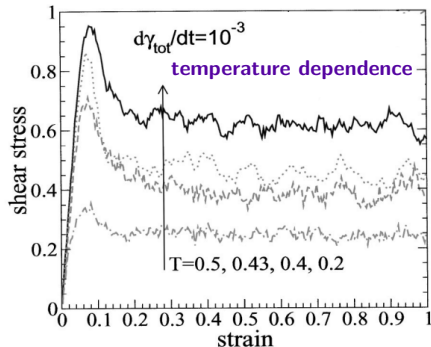
## simulations of model glasses

F. Varnik, L. Bocquet, and J.-L. Barrat, J. Chem. Phys. 120, 2788 (2004)

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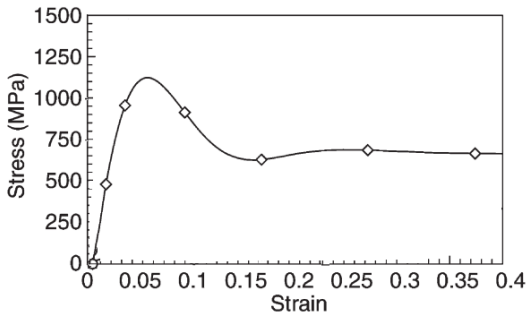




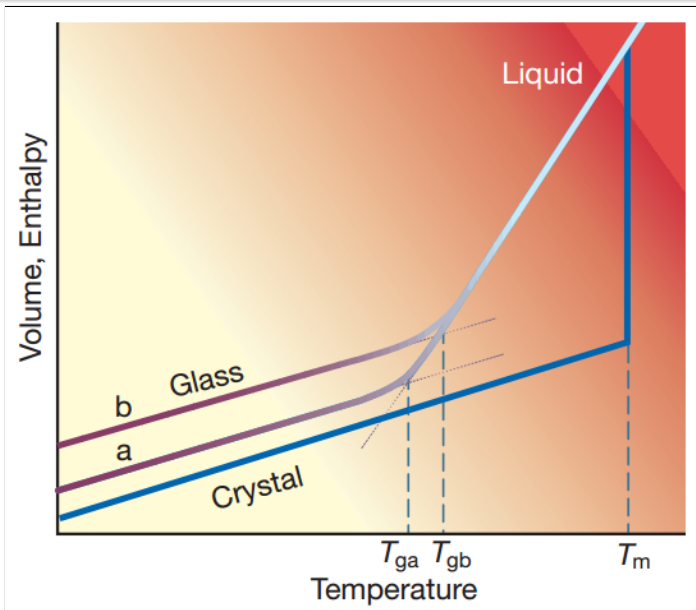
this talk: **structural** order parameters

$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, \text{???})$$

what should go here?



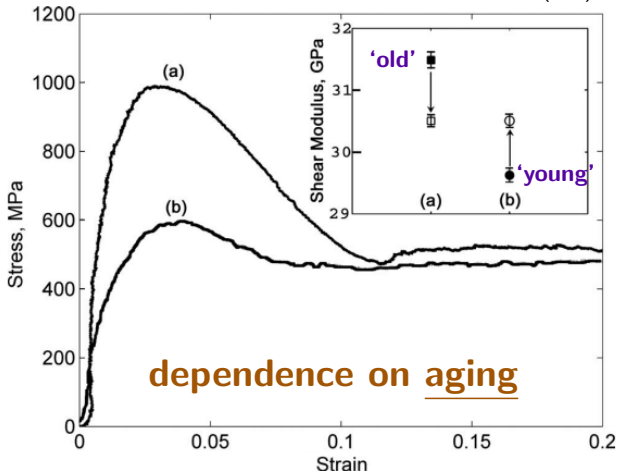
# structural order parameters? aging effects



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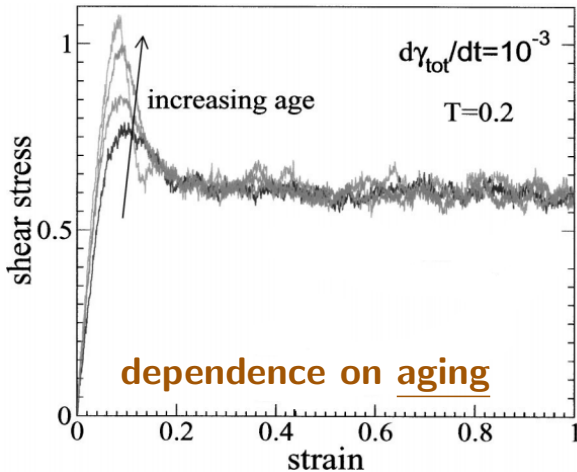
J. Lu, G. Ravichandran, W. Johnson, *Acta Materialia* 51 (2003)



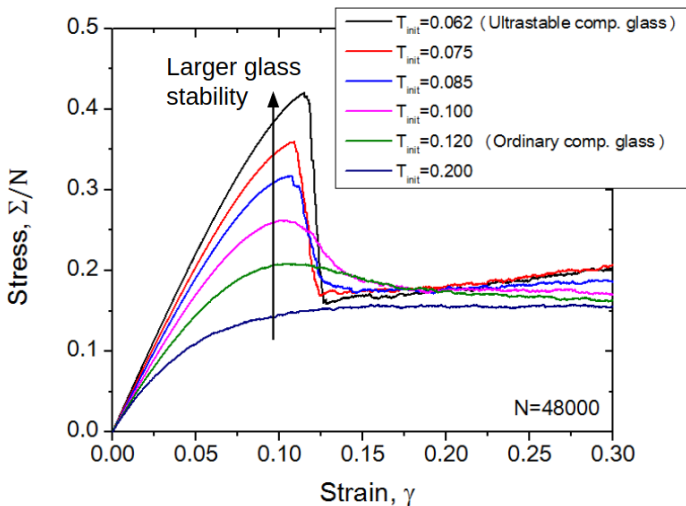
## structural order parameters? aging effects

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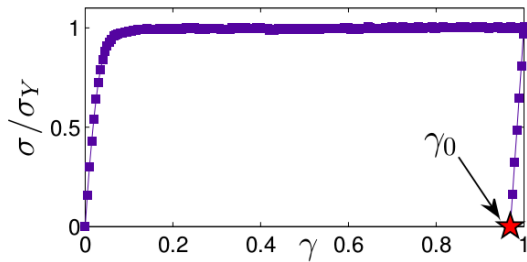
## structural order parameters? aging effects



many thanks to Misaki Ozawa!

# structural order parameters? anisotropy

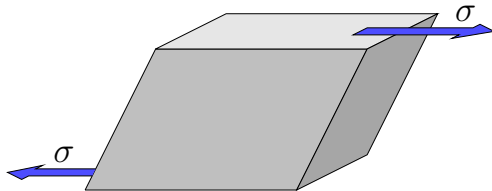
$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, ???)$$



simulations @

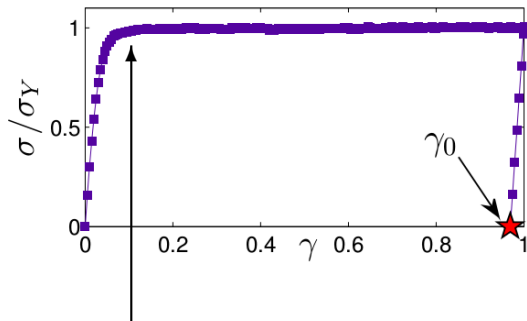
$$T \rightarrow 0$$

$$\dot{\gamma} \rightarrow 0$$



# structural order parameters? anisotropy

$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, ???)$$



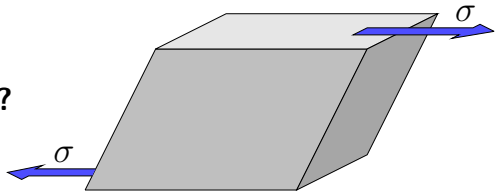
no stress overshoot

$\Rightarrow$  does structure evolve?

simulations @

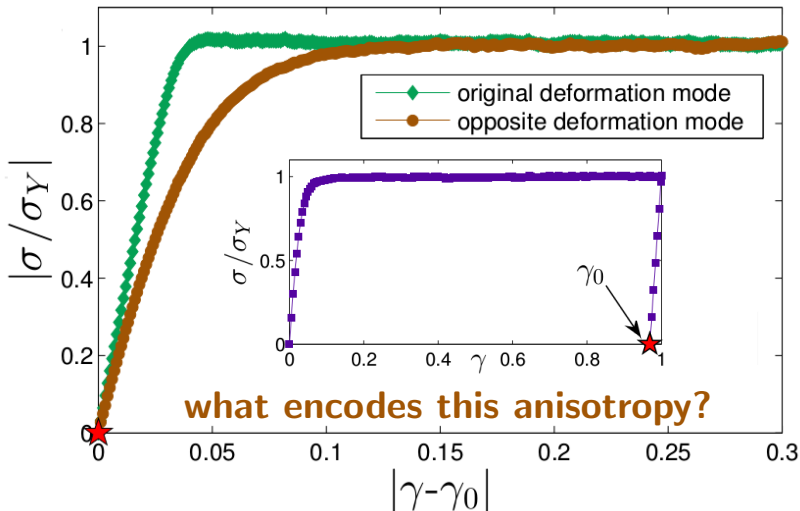
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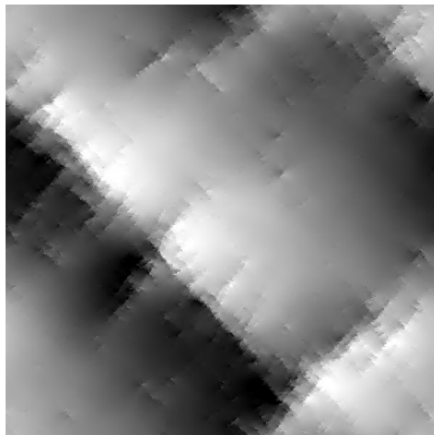
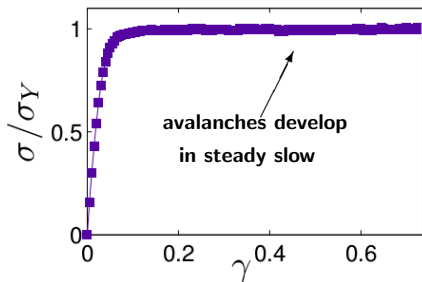
$$\frac{d\sigma}{dt} = f(\sigma, \cancel{\gamma}, \cancel{T}, \textcircled{???})$$





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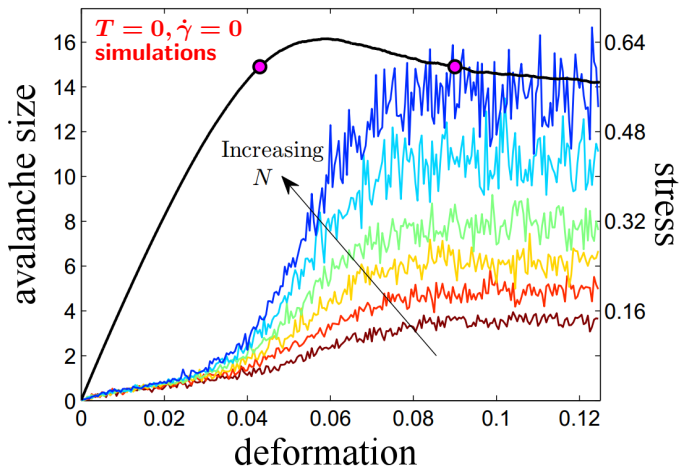
$T = 0, \dot{\gamma} = 0$   
simulations



# structural order parameters? development of avalanches

$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, ???)$$

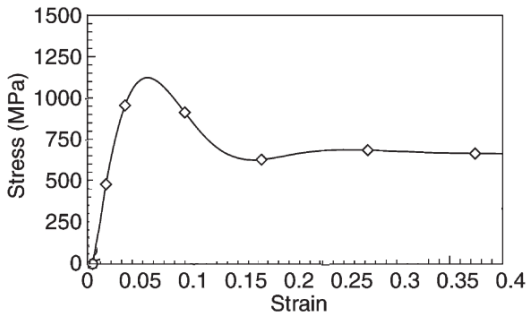
S. Karmakar, EL, and I. Procaccia, Phys. Rev. E 82, 055103(R) (2010).



## structural order parameters

$$\frac{d\sigma}{dt} = f(\sigma, \dot{\gamma}, T, \text{???})$$

what should go here?

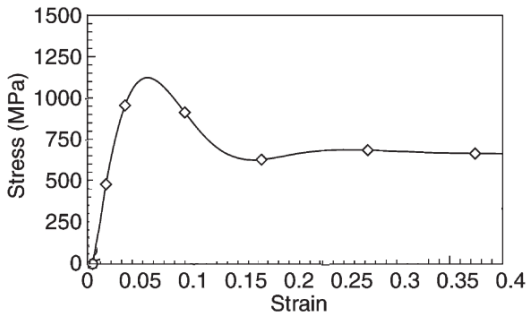


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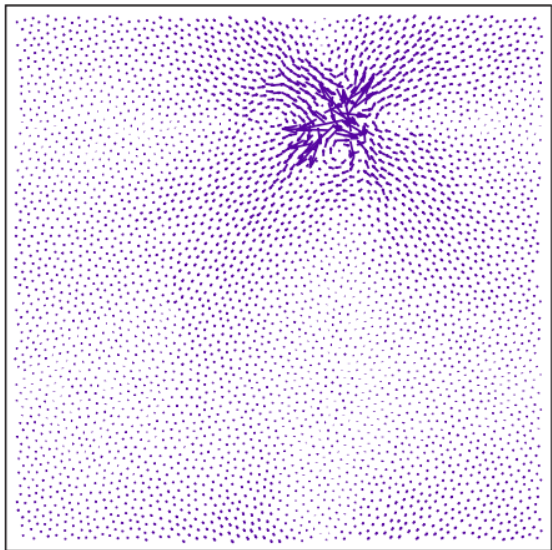
what should go here?

what actually is  $p(x)$   
from elasto-plastic models?



**what is plasticity on the micro-scale?**

## what is plasticity on the micro-scale?



**'shear-  
transformation'**

**or**

**'shear-  
transformation-  
zone'**

## how are plastic instabilities triggered?

VOLUME 93, NUMBER 19

PHYSICAL REVIEW LETTERS

week ending  
5 NOVEMBER 2004

### Universal Breakdown of Elasticity at the Onset of Material Failure

Craig Maloney<sup>1,2</sup> and Anaël Lemaître<sup>1,3</sup>

<sup>1</sup>*Department of Physics, University of California, Santa Barbara, California 93106, USA*

<sup>2</sup>*Lawrence Livermore National Lab, CMS-MSTD, Livermore, California 94550, USA*

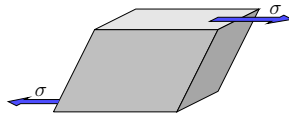
<sup>3</sup>*LMDH, Université Paris VI, UMR 7603, 4 place Jussieu, 75005 Paris, France*

(Received 6 May 2004; published 2 November 2004)

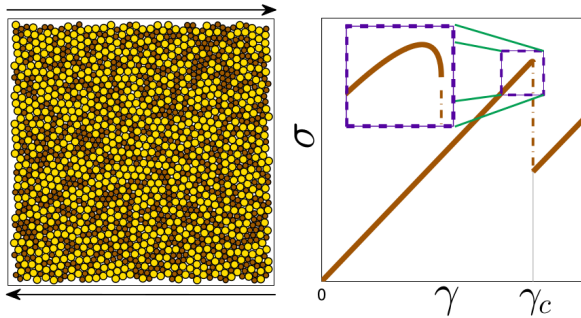
‘energy landscape’ picture:



increase imposed deformation  $\longrightarrow$

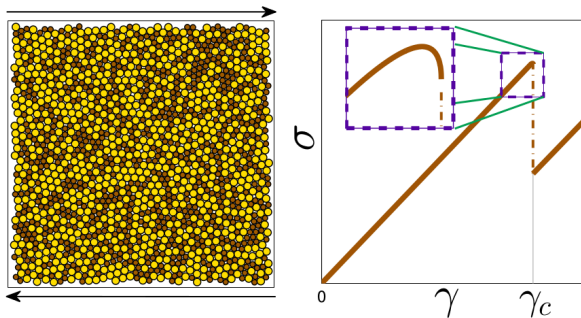


# micromechanics of plastic instabilities





# micromechanics of plastic instabilities

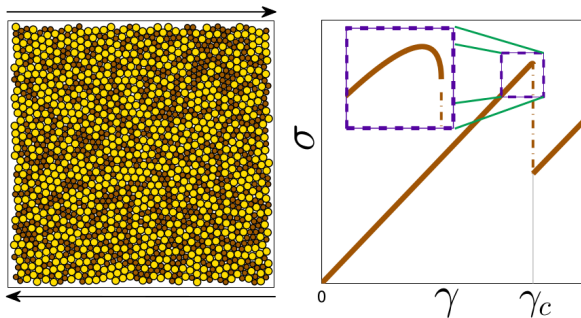


consider linear stability

$$\mathcal{M}_{jk} \equiv \frac{\partial^2 U}{\partial \vec{x}_j \partial \vec{x}_k}$$

dynamical matrix / hessian

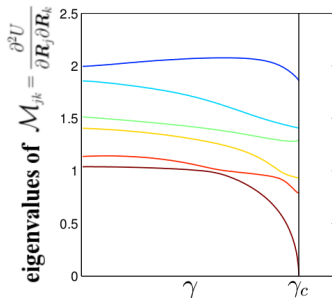
# micromechanics of plastic instabilities



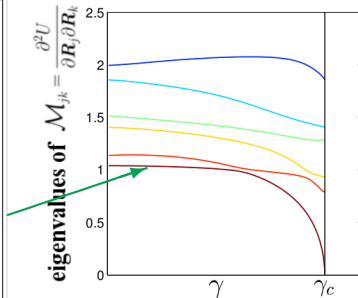
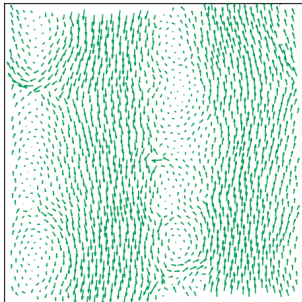
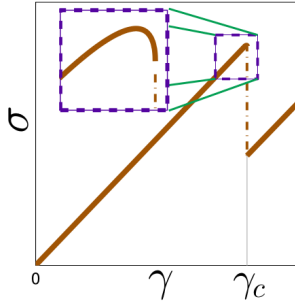
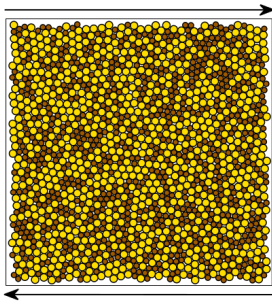
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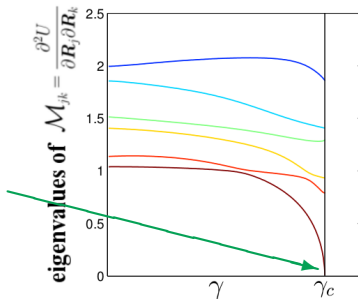
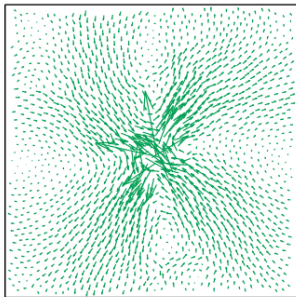
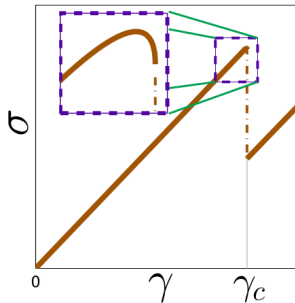
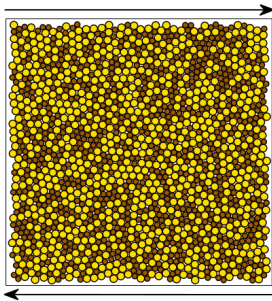
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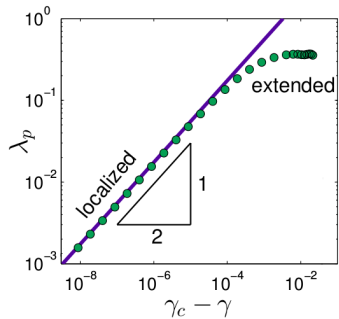
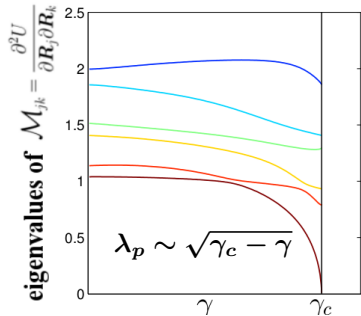
# micromechanics of plastic instabilities



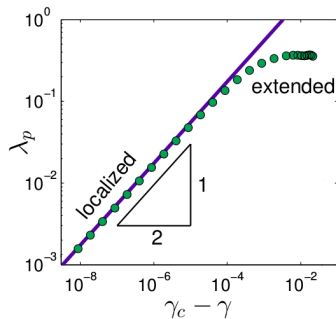
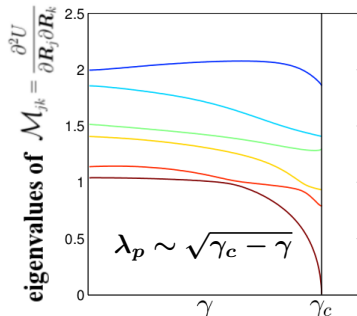
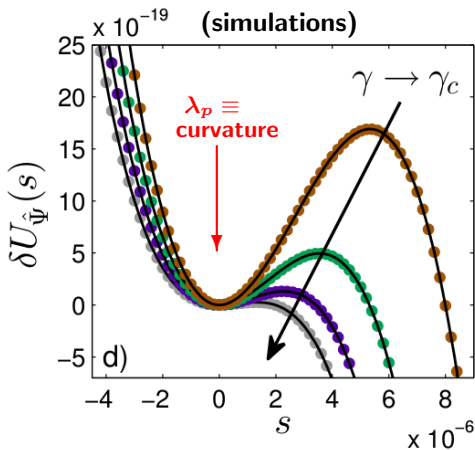
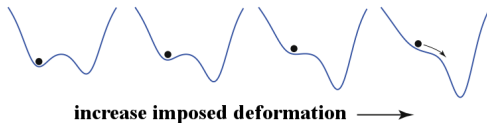
# micromechanics of plastic instabilities



# micromechanics of plastic instabilities



# micromechanics of plastic instabilities



# predicting plastic instabilities using normal modes

observation: 'linear' (normal) modes are indicative of plastic instabilities.

# **predicting plastic instabilities using normal modes**

observation: 'linear' (normal) modes are indicative of plastic instabilities.

proposition: use normal modes to detect 'soft spots'



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A LETTERS JOURNAL EXPLORING  
THE FRONTIERS OF PHYSICS

April 2010

EPL, **90** (2010) 16004

[www.epljournal.org](http://www.epljournal.org)

doi: 10.1209/0295-5075/90/16004

## Vibrational modes as a predictor for plasticity in a model glass

A. TANGUY<sup>(a)</sup>, B. MANTISI and M. TSAMADOS

*Université de Lyon - F-69622, Lyon, France, EU and  
CNRS, UMR5586, Laboratoire de Physique de la Matière Condensée et des Nanostructures, Université Lyon 1  
F-69622, Villeurbanne Cedex, France, EU*

PRL **107**, 108302 (2011)

PHYSICAL REVIEW LETTERS

week ending  
2 SEPTEMBER 2011

## Vibrational Modes Identify Soft Spots in a Sheared Disordered Packing

M. L. Manning\*

*Princeton Center for Theoretical Science, Princeton, New Jersey 08544, USA  
Department of Physics, Syracuse University, Syracuse, New York 13244, USA*

A. J. Liu

*Department of Physics, University of Pennsylvania, Philadelphia, Pennsylvania 19130, USA  
(Received 21 December 2010; published 31 August 2011)*

PHYSICAL REVIEW E **89**, 042304 (2014)

## Predicting plasticity with soft vibrational modes: From dislocations to glasses

Jörg Rottler,<sup>1</sup> Samuel S. Schoenholz,<sup>2</sup> and Andrea J. Liu<sup>2</sup>

<sup>1</sup>*Department of Physics and Astronomy, University of British Columbia, 6224 Agricultural Road,  
Vancouver, British Columbia, Canada V6T 1Z4*

<sup>2</sup>*Department of Physics, University of Pennsylvania, Philadelphia, Pennsylvania 19130, USA  
(Received 19 December 2013; revised manuscript received 26 February 2014; published 14 April 2014)*

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observation: 'linear' (normal) modes are indicative of plastic instabilities.

proposition: use normal modes to detect 'soft spots'

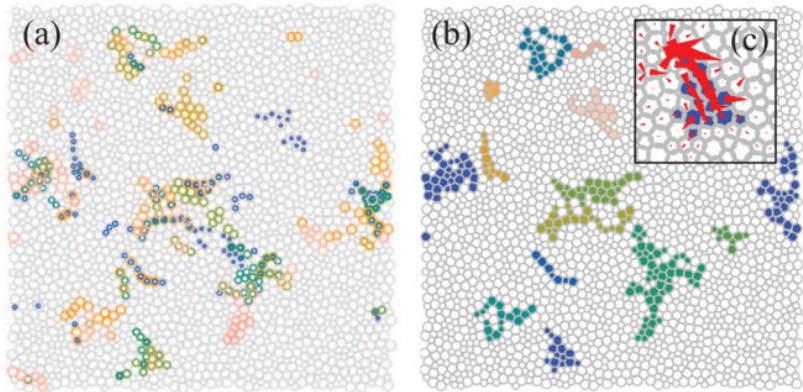
problems:

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problems: 1) no quantitative information

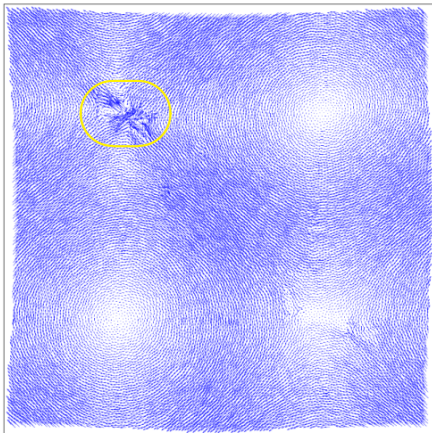


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problems: 2) hybridizations with plane waves



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## problems: 2) hybridizations with plane waves

compare lowest energy

plane wave freq.  $\omega^2 \sim 1/L^2$

with  $\lambda_p \sim \sqrt{\gamma_c - \gamma}$

$$\Rightarrow \gamma_c - \gamma \sim L^{-4}$$

dehybridization strain scale

# predicting plastic instabilities using normal modes

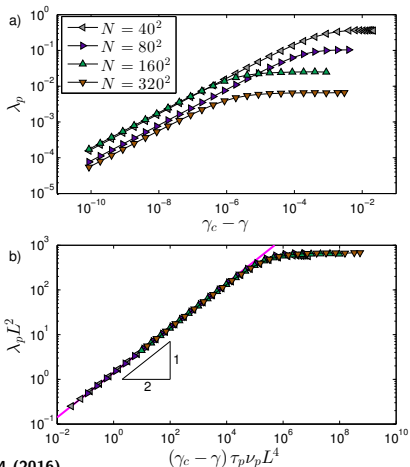
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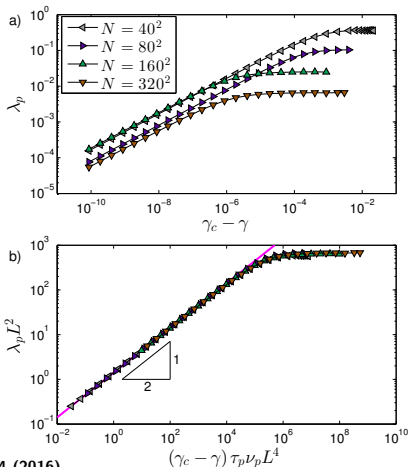
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**problematic as  $L$  increases...**



predicting plastic instabilities – can we do better?

is there a way to define and detect  
plastic modes far from instability strains,  
deep in the hybridized regime?



## **predicting plastic instabilities – can we do better?**

**yes**

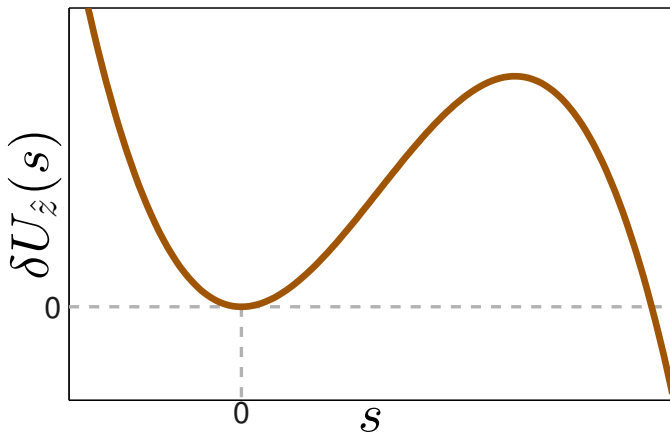
**probably**  
(TBD...)

**is there a way to define and detect  
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## the barrier function – definition

consider the energy variation upon displacing particles' coordinates  $\vec{x}$  according to  $\delta\vec{x} = s\hat{z}$

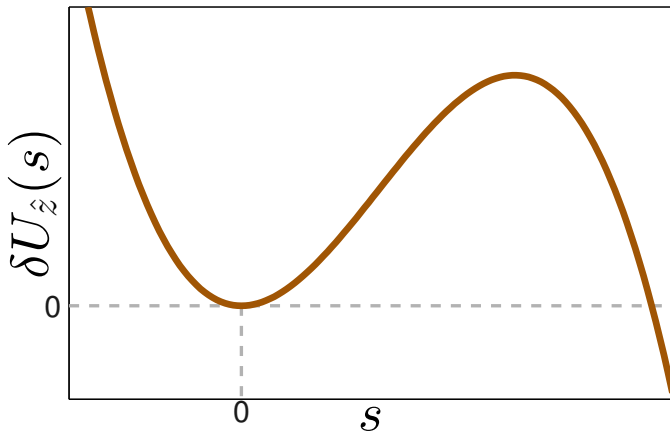
$$\delta U_{\hat{z}}(s) \simeq \frac{1}{2}\kappa_{\hat{z}}s^2 + \frac{1}{6}\tau_{\hat{z}}s^3$$



## the barrier function – definition

consider the energy variation upon displacing particles' coordinates  $\vec{x}$  according to  $\delta\vec{x} = s\hat{z}$  ↗  $\hat{z}$  not necessarily a normal mode!

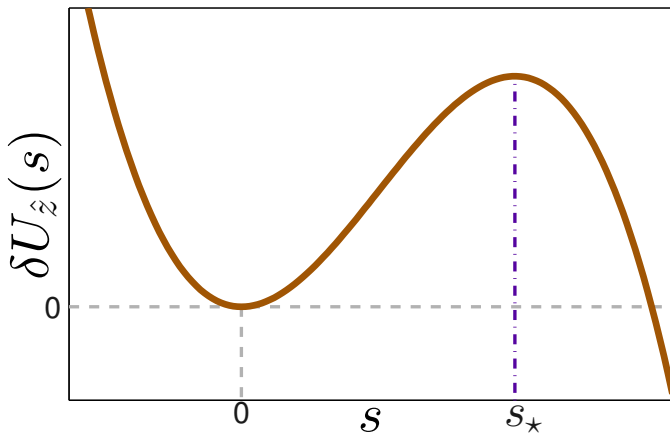
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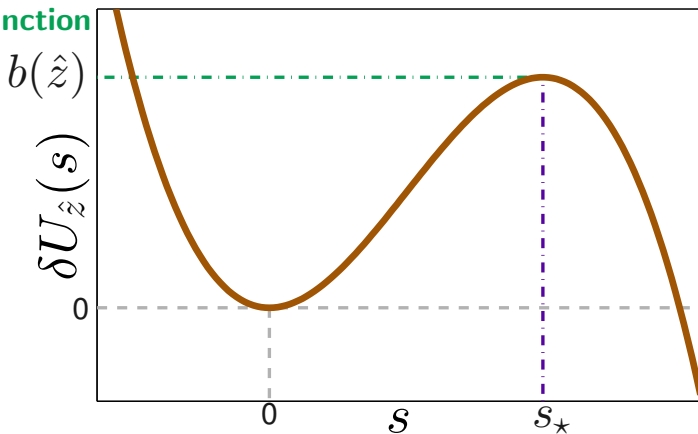


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barrier  
function



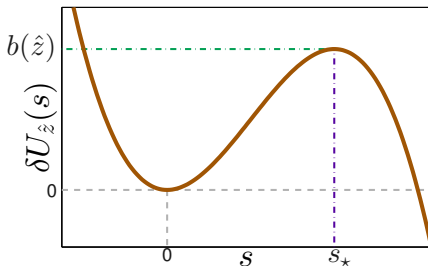
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barrier  
function

$$\delta U_{\hat{z}}(s) \simeq \frac{1}{2}\kappa_{\hat{z}}s^2 + \frac{1}{6}\tau_{\hat{z}}s^3$$

$$b(\hat{z}) \equiv \delta U_{\hat{z}}(s_{\star}) = \frac{2\kappa_{\hat{z}}^3}{3\tau_{\hat{z}}^2} = \frac{2}{3} \frac{(\mathcal{M} : \hat{z}\hat{z})^3}{(U''' : \hat{z}\hat{z}\hat{z})^2}$$



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barrier  
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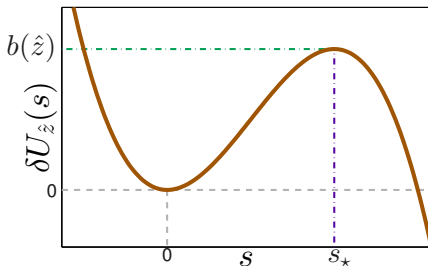
$$\delta U_{\hat{z}}(s) \simeq \frac{1}{2}\kappa_{\hat{z}}s^2 + \frac{1}{6}\tau_{\hat{z}}s^3$$

$$b(\hat{z}) \equiv \delta U_{\hat{z}}(s_{\star}) = \frac{2\kappa_{\hat{z}}^3}{3\tau_{\hat{z}}^2} = \frac{2}{3} \frac{(\mathcal{M} : \hat{z}\hat{z})^3}{(U''' : \hat{z}\hat{z}\hat{z})^2}$$

shorthand notations:

$$\mathcal{M} \equiv \frac{\partial^2 U}{\partial \vec{x} \partial \vec{x}} \quad \text{'dynamical matrix'}$$

$$U''' \equiv \frac{\partial^3 U}{\partial \vec{x} \partial \vec{x} \partial \vec{x}} \quad \text{'cubic tensor'}$$



# the barrier function – definition

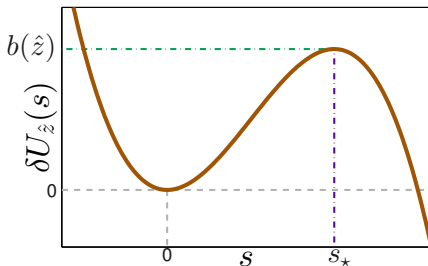
consider the energy variation upon displacing particles' coordinates  $\vec{x}$  according to  $\delta\vec{x} = s\hat{z}$  ↗  $\hat{z}$  not necessarily a normal mode!

barrier  
function

$$\delta U_{\hat{z}}(s) \simeq \frac{1}{2}\kappa_{\hat{z}}s^2 + \frac{1}{6}\tau_{\hat{z}}s^3$$

$$b(\hat{z}) \equiv \delta U_{\hat{z}}(s_{\star}) = \frac{2\kappa_{\hat{z}}^3}{3\tau_{\hat{z}}^2} = \frac{2}{3} \frac{(\mathcal{M} : \hat{z}\hat{z})^3}{(U''' : \hat{z}\hat{z}\hat{z})^2}$$

only a function of  
**inherent state information**,  
and the direction  $\hat{z}$



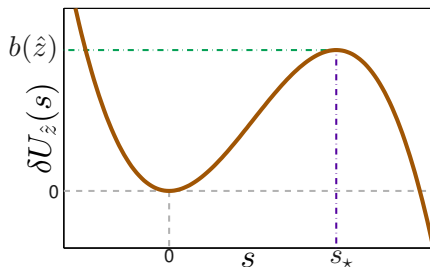


## the barrier function – definition

barrier  
function

$$b(\hat{z}) \equiv \delta U_{\hat{z}}(s_{\star}) = \frac{2}{3} \frac{\kappa_{\hat{z}}^3}{\tau_{\hat{z}}^2} = \frac{2}{3} \frac{(\mathcal{M} : \hat{z}\hat{z})^3}{(U''' : \hat{z}\hat{z}\hat{z})^2}$$

directions  $\hat{z}$  which take the system over  
low saddle points will have small  $b(\hat{z})$ 's



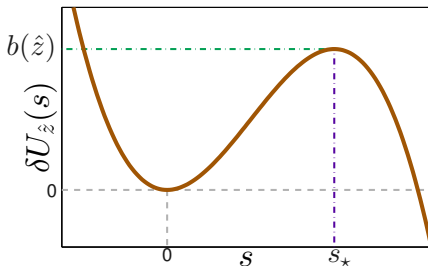
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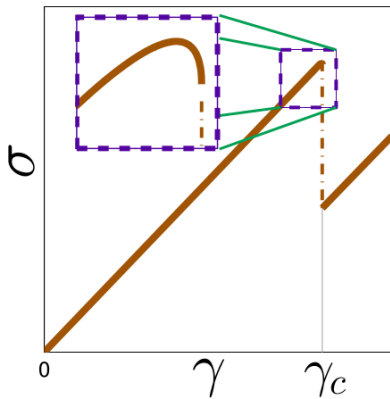
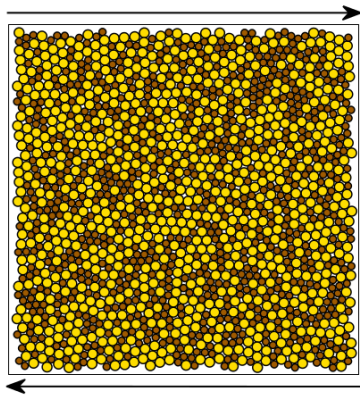
directions  $\hat{z}$  which take the system over  
low saddle points will have small  $b(\hat{z})$ 's

$\Rightarrow$  find directions with  
small  $b(\hat{z})$  by minimizing  
 $b(\hat{z})$  over directions  $\hat{z}$



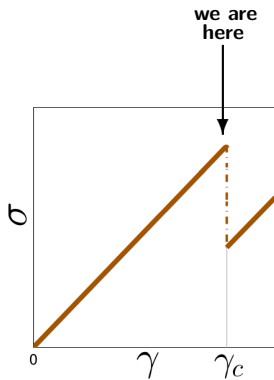
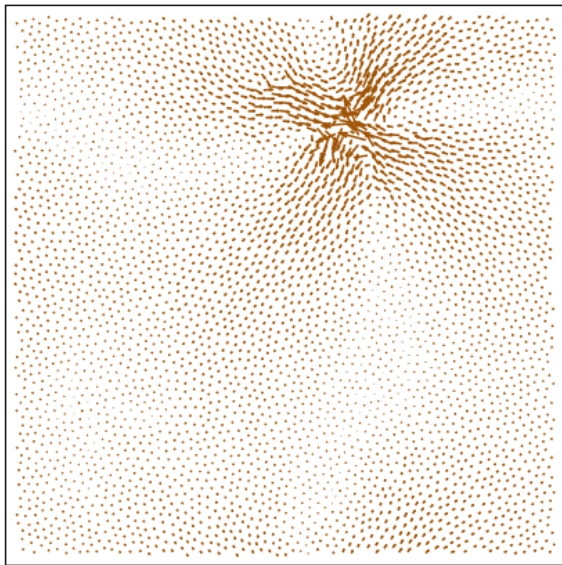
# finding small $b(\hat{z})$ 's

setup:



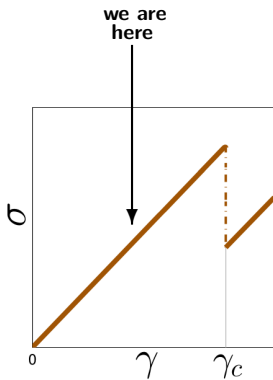
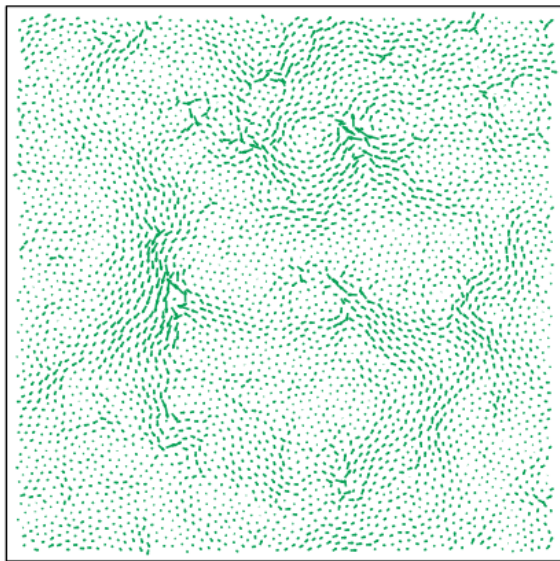
# finding small $b(\hat{z})$ 's

destabilizing **linear** mode  $\hat{\Psi}_p$ ,  $\gamma \rightarrow \gamma_c$



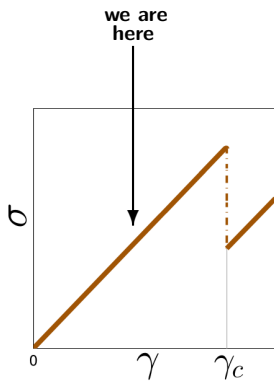
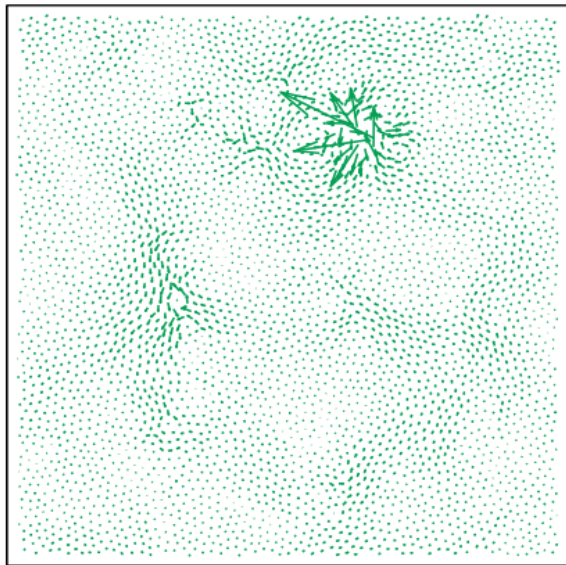
## finding small $b(\hat{z})$ 's

linear response to shear,  $\gamma_c - \gamma \sim 10^{-2}$ , use as initial guess  $\hat{z}_{\text{ini}}$



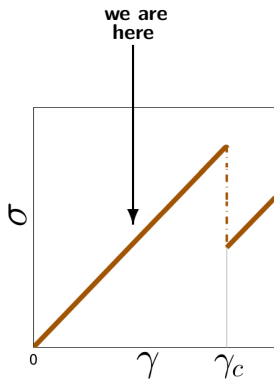
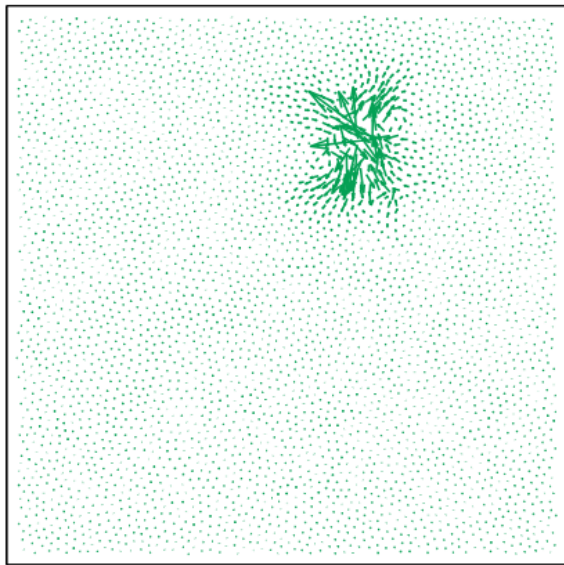
# finding small $b(\hat{z})$ 's

minimize  $b(\hat{z})$ , after 12 iterations,  $\gamma_c - \gamma \sim 10^{-2}$



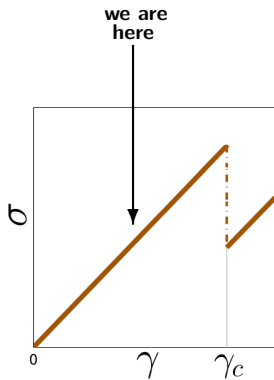
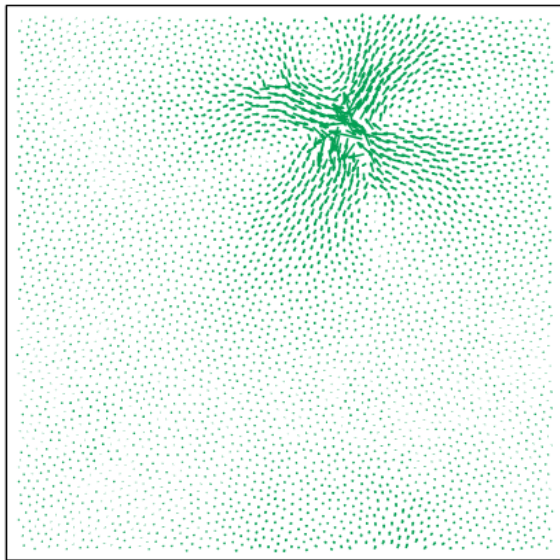
# finding small $b(\hat{z})$ 's

minimize  $b(\hat{z})$ , after 24 iterations,  $\gamma_c - \gamma \sim 10^{-2}$



# finding small $b(\hat{z})$ 's

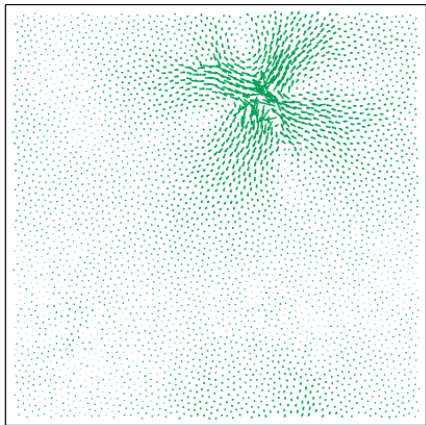
minimization converged,  $\gamma_c - \gamma \sim 10^{-2}$



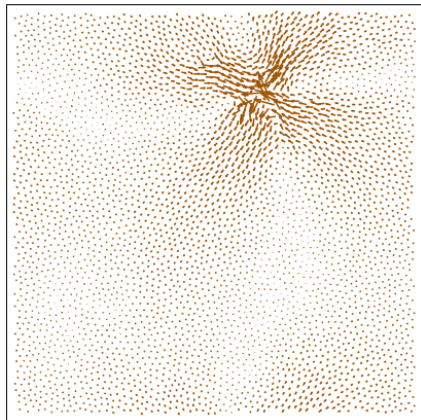


# finding small $b(\hat{z})$ 's

direction  $\hat{z}$  that **minimizes**  $b(\hat{z})$   
 $\gamma_c - \gamma \sim 10^{-2}$



destabilizing **linear** mode  $\hat{\Psi}_p$   
 $\gamma_c - \gamma \sim 10^{-7}$

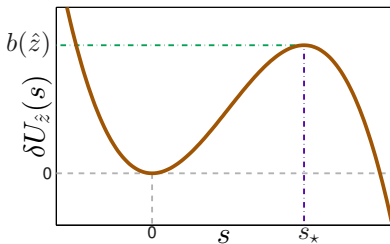


## nonlinear plastic modes – definition

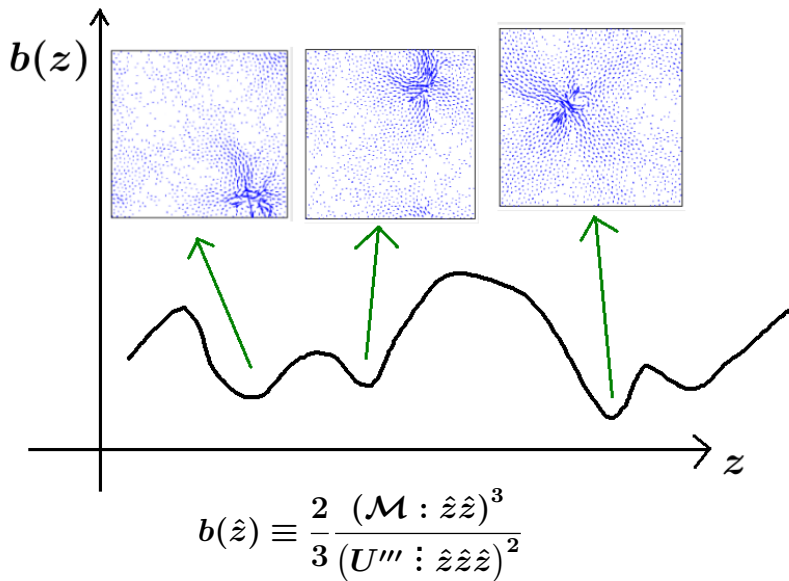
**nonlinear plastic modes** are collective displacement directions  $\hat{\pi}$  for which the barrier function  $b(\hat{z})$  displays a **local minimum**

$$\left. \frac{\partial b}{\partial \vec{z}} \right|_{\hat{\pi}} = 0, \quad \left. \frac{\partial^2 b}{\partial \vec{z} \partial \vec{z}} \right|_{\hat{\pi}} > 0$$

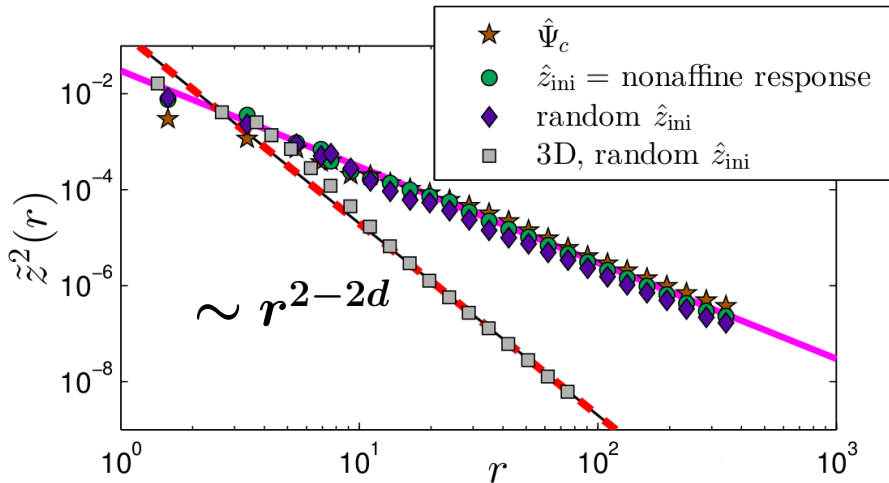
$$b(\hat{z}) \equiv \frac{2}{3} \frac{(\mathcal{M} : \hat{z}\hat{z})^3}{(U''' : \hat{z}\hat{z}\hat{z})^2}$$



## nonlinear plastic modes – illustration

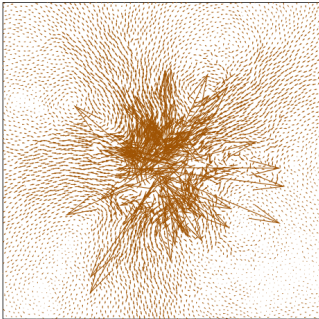
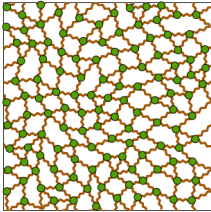


nonlinear plastic modes decay like the  
response to local perturbation  $|\hat{\pi}| \sim r^{1-d}$

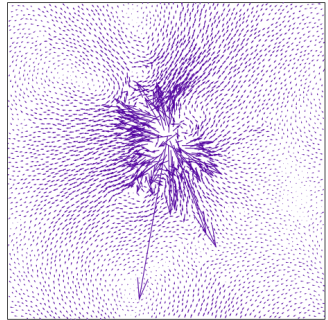
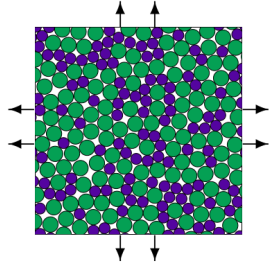


# nonlinear plastic modes – spatial structure

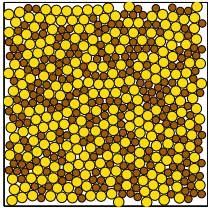
no internal stresses



glass under tension

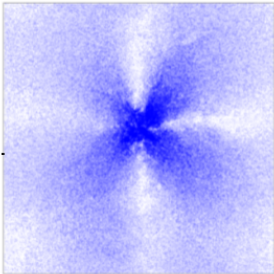


# nonlinear plastic modes – core size

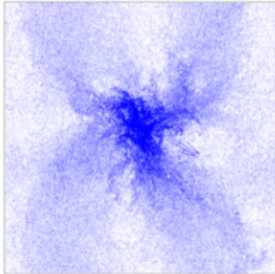


packings of harmonic discs

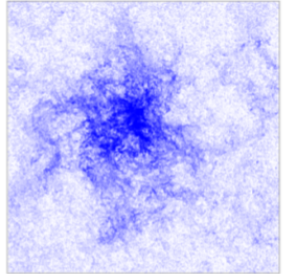
‘unjamming’



$p = 10^{-1}$

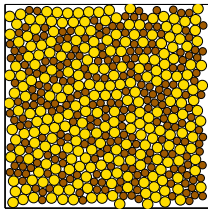


$p = 10^{-3}$



$p = 10^{-5}$

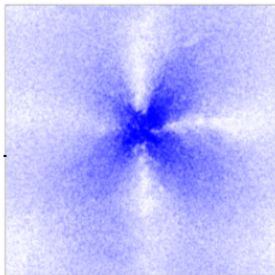
# nonlinear plastic modes – core size



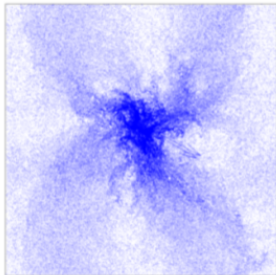
packings of harmonic discs

$$\ell_c \sim \frac{1}{\sqrt{z - z_c}} \sim p^{-1/4}?$$

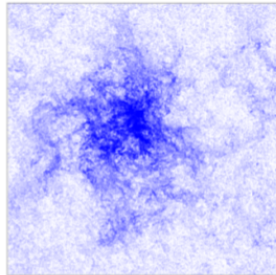
‘unjamming’



$p = 10^{-1}$



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## usefulness of nonlinear plastic modes

**nonlinear plastic modes** are collective displacement directions  $\hat{\pi}$  for which the barrier function  $b(\hat{z})$  displays a **local minimum**

$$\left. \frac{\partial b}{\partial \vec{z}} \right|_{\hat{\pi}} = 0, \quad \left. \frac{\partial^2 b}{\partial \vec{z} \partial \vec{z}} \right|_{\hat{\pi}} > 0$$

why are nonlinear plastic modes the  
**natural micromechanical objects**  
to consider in plasticity studies?



## nonlinear plastic modes – deformation dynamics

we defined  $\hat{\pi}$  via  $\left. \frac{\partial b}{\partial \vec{z}} \right|_{\hat{\pi}} = 0$

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**how do the stiffnesses  $\kappa_{\hat{\pi}}$  depend on deformation?**

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how do the stiffnesses  $\kappa_{\hat{\pi}}$  depend on deformation?

$$\frac{d\kappa_{\hat{\pi}}}{d\gamma} \simeq \frac{d\mathcal{M}}{d\gamma} : \hat{\pi} \hat{\pi} = -U''' : \hat{\pi} \hat{\pi} \left( \mathcal{M}^{-1} \cdot \frac{\partial^2 U}{\partial \vec{x} \partial \gamma} \right)$$

following  $(\star)$ :

$$= - \frac{\tau_{\hat{\pi}} \hat{\pi} \cdot \mathcal{M} \cdot \mathcal{M}^{-1} \cdot \frac{\partial^2 U}{\partial \vec{x} \partial \gamma}}{\kappa_{\hat{\pi}}}$$

$$= - \frac{\tau_{\hat{\pi}} \nu_{\hat{\pi}}}{\kappa_{\hat{\pi}}}, \quad \begin{array}{l} \tau_{\hat{\pi}} \equiv \frac{\partial^3 U}{\partial \vec{x} \partial \vec{x} \partial \vec{x}} : \hat{\pi} \hat{\pi} \hat{\pi} \text{ asymmetry} \\ \nu_{\hat{\pi}} \equiv \hat{\pi} \cdot \frac{\partial^2 U}{\partial \vec{x} \partial \gamma} \text{ shear coupling} \end{array}$$

## nonlinear plastic modes – deformation dynamics

we found a simple form for

$$\frac{d\kappa_{\hat{\pi}}}{d\gamma} \simeq -\frac{\tau_{\hat{\pi}}\nu_{\hat{\pi}}}{\kappa_{\hat{\pi}}}$$

## nonlinear plastic modes – deformation dynamics

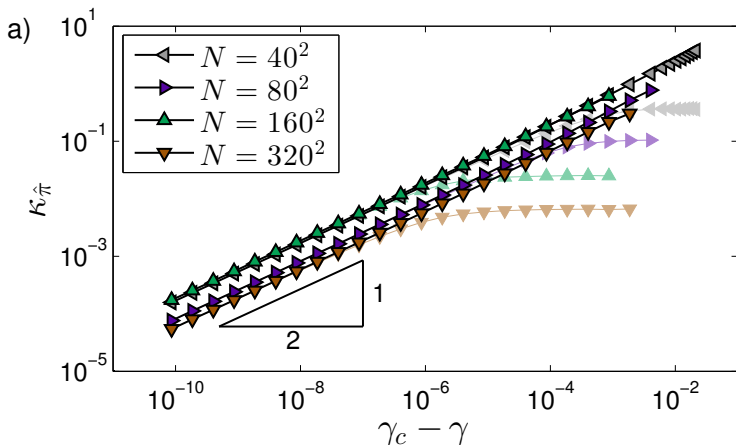
we found a simple form for  $\frac{d\kappa_{\hat{\pi}}}{d\gamma} \simeq -\frac{\tau_{\hat{\pi}}\nu_{\hat{\pi}}}{\kappa_{\hat{\pi}}}$

trivially solved as  $\kappa_{\hat{\pi}} \simeq \sqrt{2\nu_{\hat{\pi}}\tau_{\hat{\pi}}}\sqrt{\gamma_c - \gamma}$

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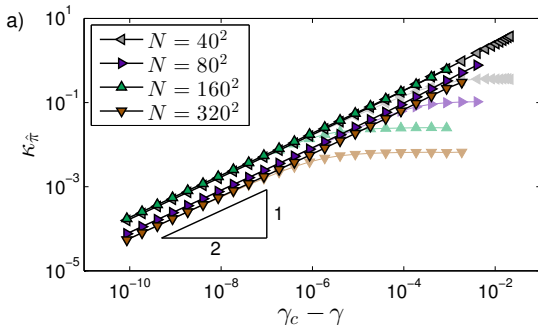
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trivially solved as  $\kappa_{\hat{\pi}} \simeq \sqrt{2\nu_{\hat{\pi}}\tau_{\hat{\pi}}} \sqrt{\gamma_c - \gamma}$

**important points:**

- 1) deformation dynamics only weakly coupled to other modes
- 2)  $N$ -independent range of validity, in stark contrast with linear modes



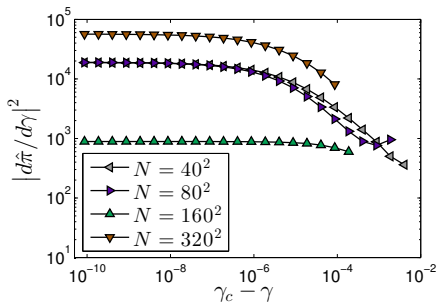


# nonlinear plastic modes – deformation dynamics

linear modes' variations are **singular**, plastic modes' are **regular**:

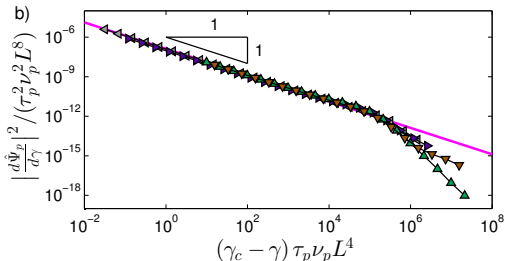
nonlinear plastic modes

$$\left| \frac{d\hat{\pi}}{d\gamma} \right| \sim \text{const.}$$



linear destabilizing mode

$$\left| \frac{d\hat{\Psi}_p}{d\gamma} \right| \sim \frac{L^2}{\sqrt{\gamma_c - \gamma}}$$



# nonlinear plastic modes – deformation dynamics

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linear destabilizing mode

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this is odd since both stiffnesses follow same EOM

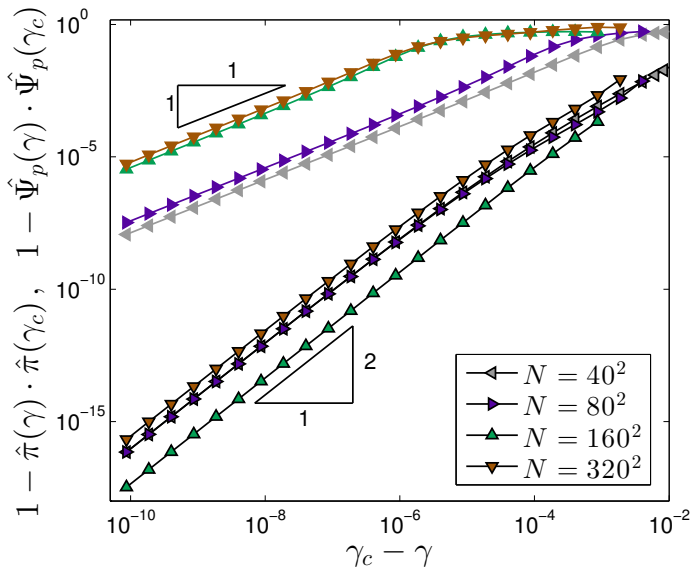
$$\frac{d\kappa}{d\gamma} \sim \frac{1}{\kappa}$$

$$(\kappa \equiv \mathcal{M} : \hat{\pi} \hat{\pi})$$

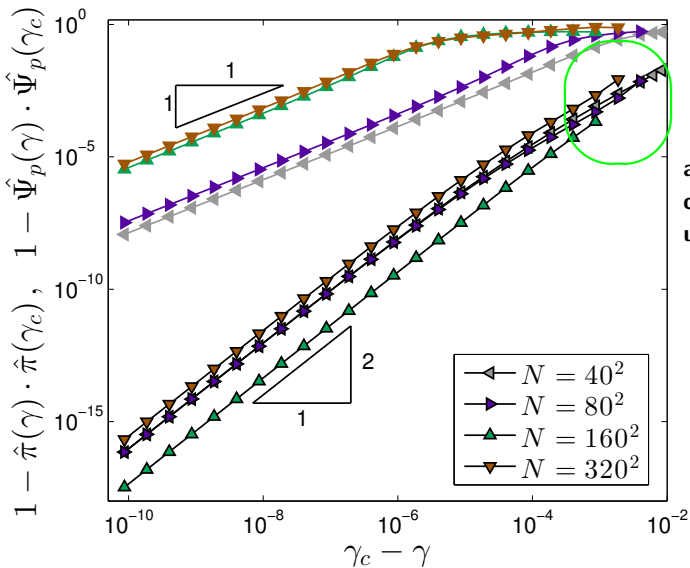
$$\frac{d\lambda_p}{d\gamma} \sim \frac{1}{\lambda_p}$$

$$(\lambda_p \equiv \mathcal{M} : \hat{\Psi}_p \hat{\Psi}_p)$$

# predictiveness of nonlinear plastic modes

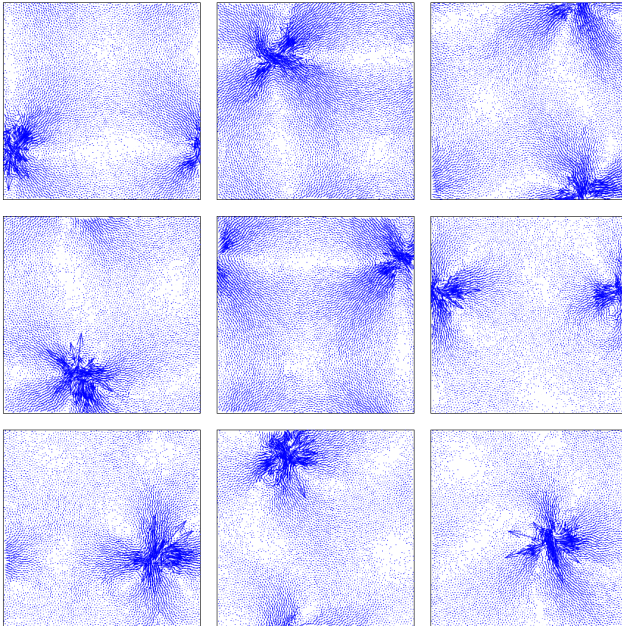


# predictiveness of nonlinear plastic modes



as soon as detected,  
overlap with instability  
up to more than 99%!

# TBD: detecting the **field** of nonlinear plastic modes



modes detected  
in a single sample

in progress...

## statistics of nonlinear plastic modes

what attributes of NPM's should we care about?

# statistics of nonlinear plastic modes

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recall: NPM's are characterized by:

- their stiffnesses  $\kappa = \frac{\partial^2 U}{\partial \vec{x} \partial \vec{x}} : \hat{\pi} \hat{\pi}$
- their asymmetries  $\tau = \frac{\partial^3 U}{\partial \vec{x} \partial \vec{x} \partial \vec{x}} \vdots \hat{\pi} \hat{\pi} \hat{\pi}$
- their deformation coupling  $\nu = \frac{\partial^2 U}{\partial \gamma \partial \vec{x}} \cdot \hat{\pi}$

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- their deformation coupling  $\nu = \frac{\partial^2 U}{\partial \gamma \partial \vec{x}} \cdot \hat{\pi}$

we can construct a **field of local destabilization strains**  $\delta\gamma_c(\hat{\pi})$ :

$$\delta\gamma_c(\hat{\pi}) = \gamma_c(\hat{\pi}) - \gamma = \frac{\kappa}{2 \frac{d\kappa}{d\gamma}} = \frac{\kappa^2}{2\nu\tau}$$

$$\left( \text{recall that } \kappa = \sqrt{2\tau\nu} \sqrt{\gamma_c - \gamma}, \text{ and } \frac{d\kappa}{d\gamma} = -\frac{\tau\nu}{\kappa} \right)$$



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  - their asymmetries  $\tau = \frac{\partial^3 U}{\partial \vec{x} \partial \vec{x} \partial \vec{x}} : \hat{\pi} \hat{\pi} \hat{\pi}$
  - their deformation coupling  $\nu = \frac{\partial^2 U}{\partial \gamma \partial \vec{x}} \cdot \hat{\pi}$
- assume  $\tau$  and  $\nu$  have non-interesting distributions, **focus on stiffnesses  $\kappa$**

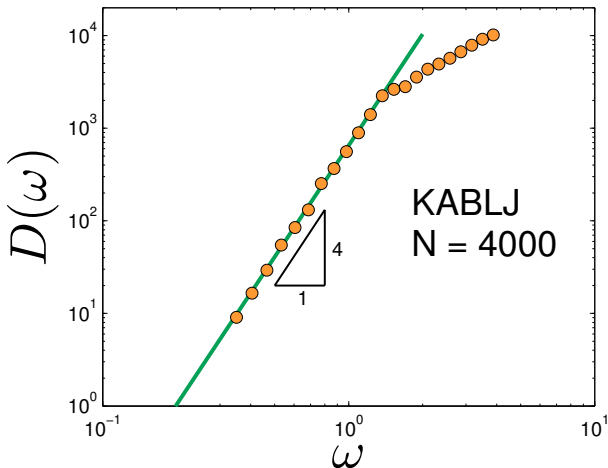
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## how are NPM stiffnesses $\kappa$ distributed?

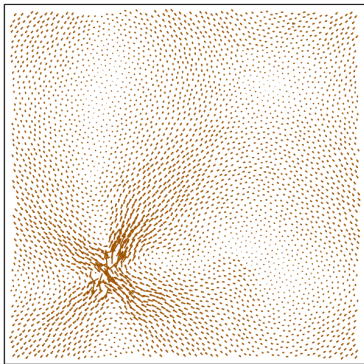
it was recently observed that a **universal** distribution  $D(\omega) \sim \omega^4$  of quasi-localized **glassy modes** appears at low frequencies



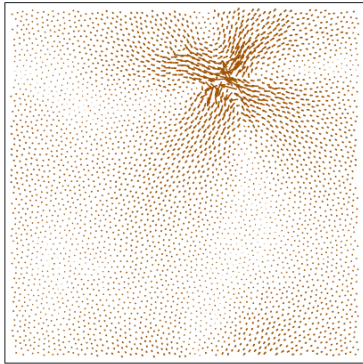
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**harmonic** glassy mode  
in **undeformed** sample



plastic instability  
upon imposing **shear**



## how are NPM stiffnesses $\kappa$ distributed?

recall we assume that strain couplings  $\nu$  and asymmetries  $\tau$  have **characteristic** ( $\kappa$  independent) values, then we expect

$$p(\kappa) \sim \kappa^{3/2} \quad \Rightarrow \quad p(\delta\gamma_c) \sim \delta\gamma_c^{1/4}$$

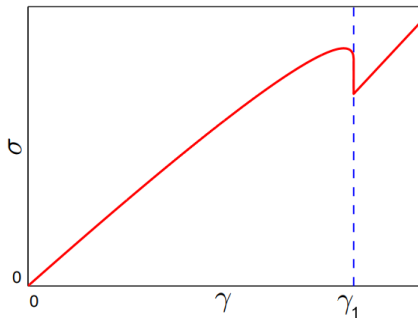
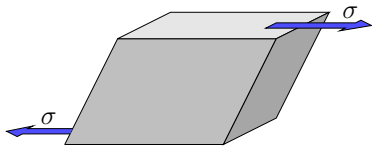
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assume now different NPMs are independent, then we expect

$$\gamma_1(N) \sim N^{-\frac{4}{5}}$$



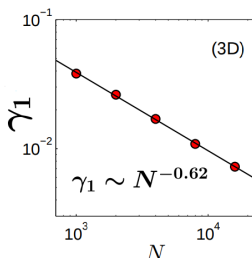
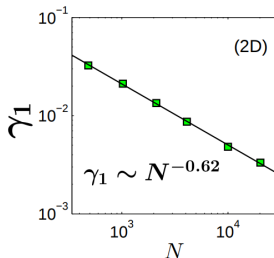
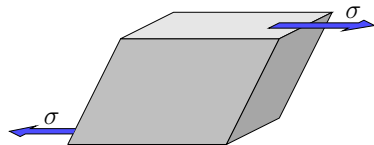
# extent of first elastic branch

recall we assume that strain couplings  $\nu$  and asymmetries  $\tau$  have **characteristic** ( $\kappa$  independent) values, then we expect

$$p(\kappa) \sim \kappa^{3/2} \quad \Rightarrow \quad p(\delta\gamma_c) \sim \delta\gamma_c^{1/4}$$

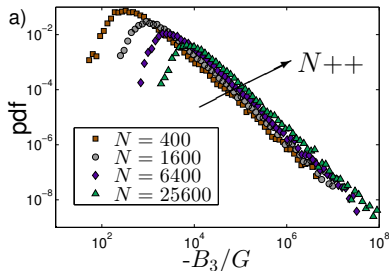
assume now different NPMs are independent, then we expect

$$\gamma_1(N) \sim N^{-\frac{4}{5}}$$



# finite-size scaling of nonlinear elasticity

a similar discrepancy appears for nonlinear elastic moduli

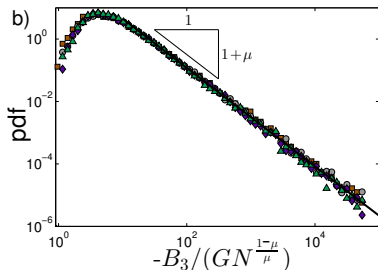


$$B_3 \equiv \frac{d^3 \sigma}{d\gamma^3}$$

we find  $\mu \approx 0.57$ ,

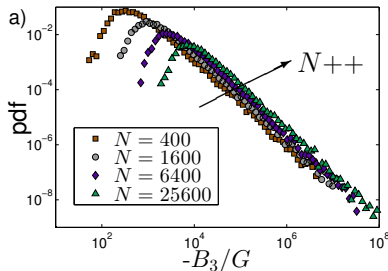
whereas  $D(\omega) \sim \omega^4$

implies  $\mu = 1/2$



# finite-size scaling of nonlinear elasticity

a similar discrepancy appears for nonlinear elastic moduli



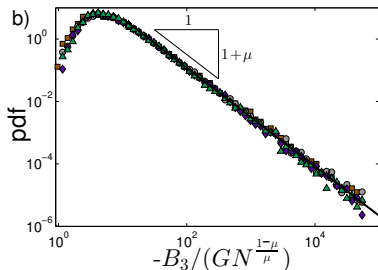
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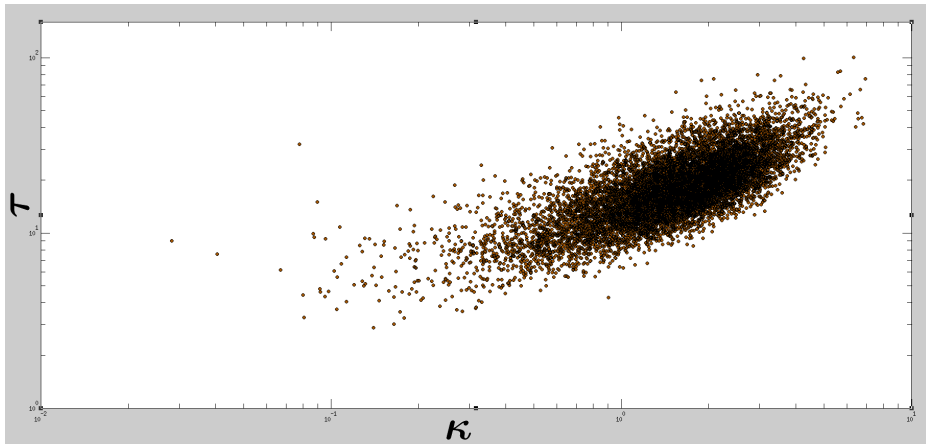
**asymmetries should depend  
on stiffnesses**





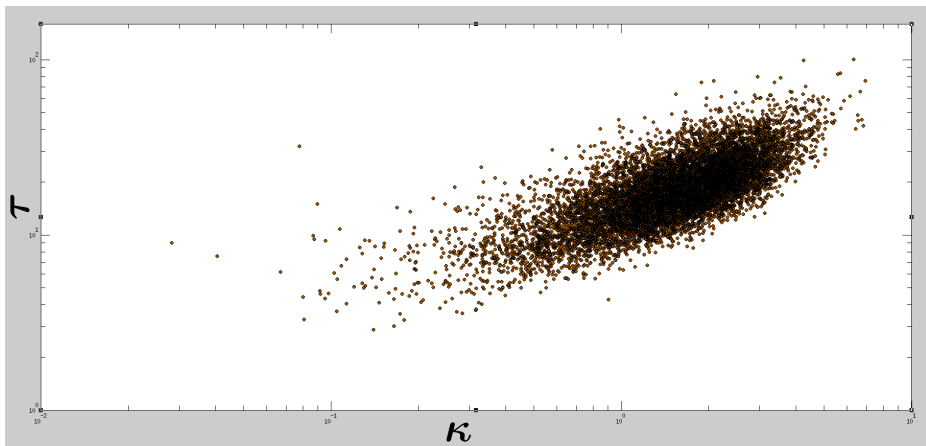
# dependence of asymmetries on stiffnesses

data measured for low-energy NPMs in 3D with  $N = 2000$



# dependence of asymmetries on stiffnesses

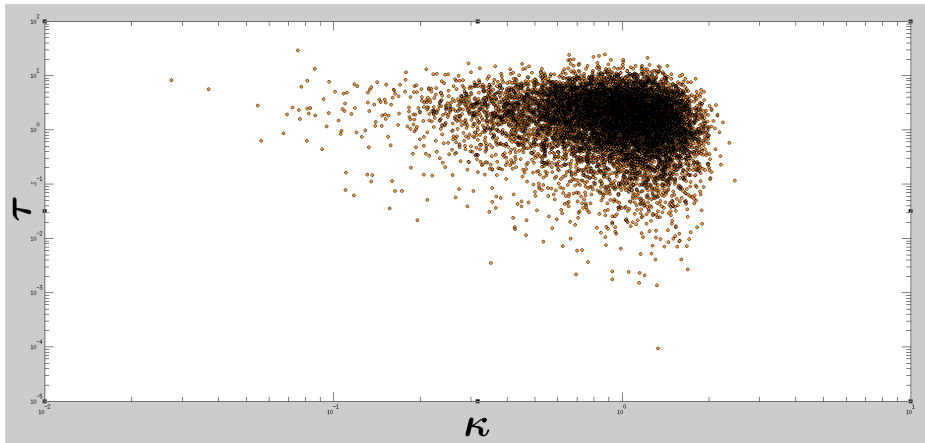
data measured for low-energy NPMs in 3D with  $N = 2000$



does this trend persist to  $\kappa \rightarrow 0$ ?

# dependence of asymmetries on stiffnesses

data measured for low-energy **harmonic modes** in 3D with  $N = 2000$

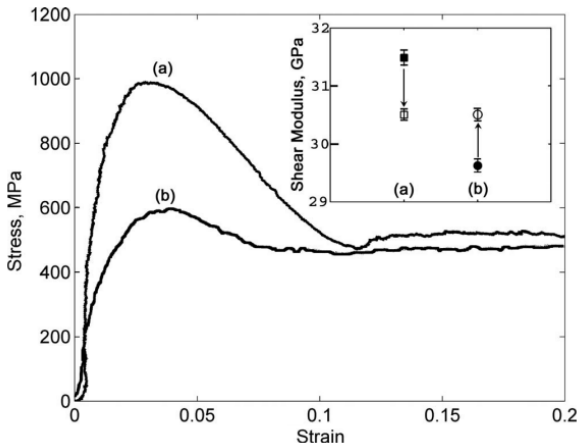


asymmetries appear to be **stiffness independent** for harmonic modes, but **not** for plastic modes

## summary: nonlinear plastic modes

- understanding elasto-plasticity and yielding requires the proper identification of the relevant structural state variables

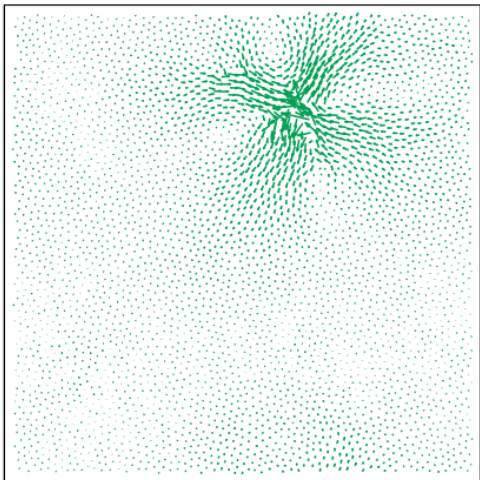
J. Lu, G. Ravichandran, W. Johnson, *Acta Materialia* 51 (2003)



## summary: nonlinear plastic modes

- NPMs offer a robust **micromechanical** definition of plasticity carriers, based solely on **inherent state information**

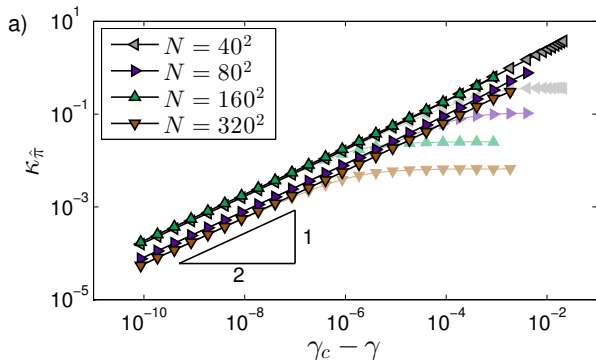
$$\left. \frac{\partial b}{\partial \vec{z}} \right|_{\hat{\pi}} = 0$$



## summary: nonlinear plastic modes

- deformation dynamics of NPMs:  $N$ -independent, no hybridizations

$$\frac{d\kappa}{d\gamma} \simeq -\frac{\tau \nu}{\kappa}$$



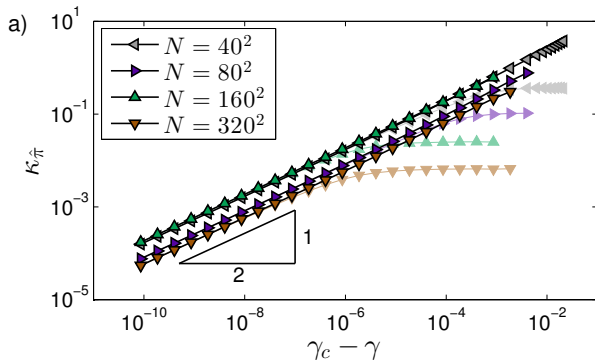
# summary: nonlinear plastic modes

- deformation dynamics of NPMs:  $N$ -independent, no hybridizations

asymmetry

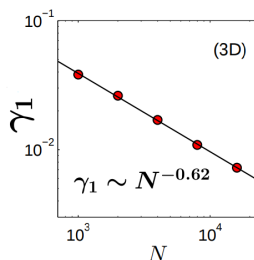
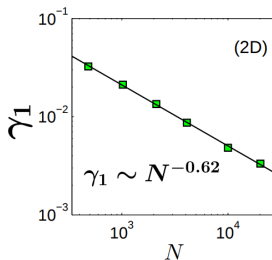
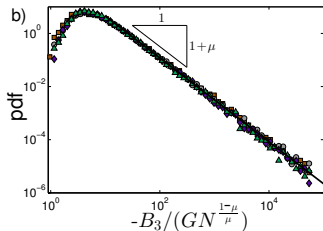
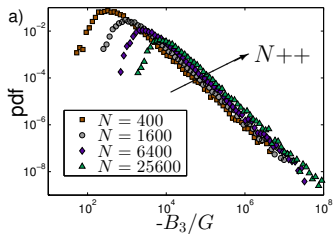
deformation coupling

$$\frac{d\kappa}{d\gamma} \simeq - \frac{\tau \nu}{\kappa}$$



# summary: nonlinear plastic modes

- still something left to understand regarding the statistics of NPMs, and the stiffness-dependence of asymmetries & deformation coupling





Ph.D. & postDoc positions available!

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thanks for your attention! questions?

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